



Data analysis of equivalence principle test in space.

Advantage of measurements in 2D

&
sensitivity of the laboratory prototype

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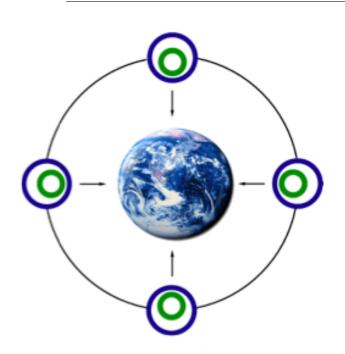


μSCOPE Colloquium III, Onera





GG: violation signal in 2D



Satellite passively stabilized by one-axis rotation at $\nu_{spin} = 1$ Hz around symmetry axis perpendicular to sensitive plane of test cylinders (blue & green indicate different composition).

Spin axis remains fixed in space (spin angular momentum conservation, very high spin energy).

Violation signal is a vector pointing to CM of Earth as the satellite orbits around it at $\nu_{orb} \simeq 1.7 \cdot 10^{-4} \, \mathrm{Hz}$

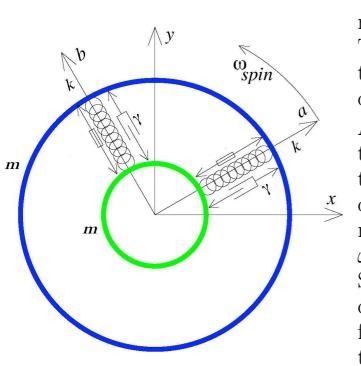








GG sensor: 2D rotating differential accelerometer



Two test cylinders of different composition rotate with the satellite at $\nu_{spin} = 1$ Hz. They are weakly coupled in the plane \perp to the spin/symmetry axis to sense tiny differential accelerations.

A co-rotating read-out (laser gauge) reads the relative (differential) displacements of the test cylinders, which provide the differential acceleration through the measured natural differential frequency ω_{diff} .

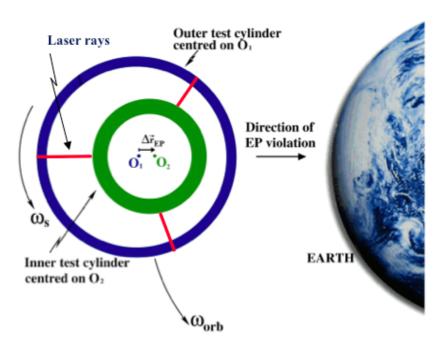
 ω_{diff} . Sensitivity $\propto 1/\omega_{diff}^2$; the weaker the coupling, the lower the differential frequency, the higher the differential period, the higher the sensitivity to differential accelerations.







GG: up-conversion of signal to high frequency



Spin of test cylinders & laser gauge read-out up-converts the violation signal vector from orbital frequency to spin frequency.

Signal frequency increased by factor $T_{orb}/T_{spin} \simeq 5800$

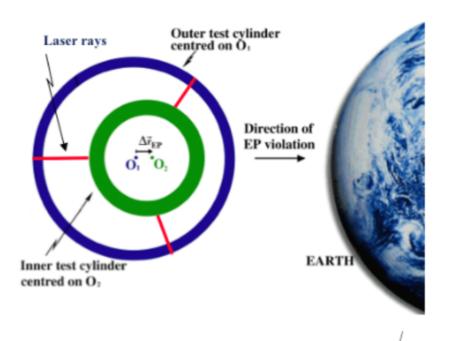








Violation signal in the non rotating satellite frame



In the satellite frame centered on TM1 & not spinning the Earth orbits at $-\omega_{orb}$ (if spin and orbital angular velocity vectors have same sign) and the violation signal points to its CM (or away from it; sign of violation unknown).

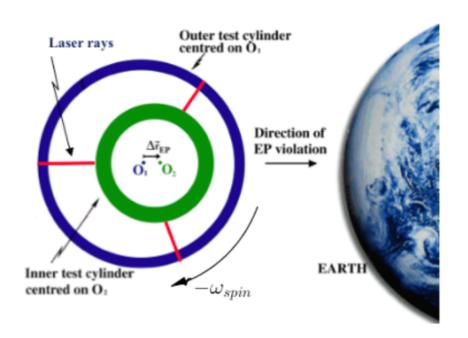








Violation signal in the rotating satellite frame



In the satellite frame centered on TM1 & spinning the violation vector rotates at $-\omega_{spin} - \omega_{orb}$.

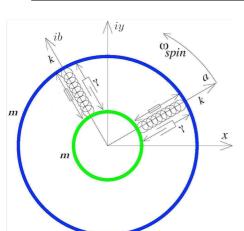
In 2D a rotating vector can be distinguished from an oscillating one with the same frequency







Complex Fourier analysis and separation of effects



2D rotating read-out gives relative displacement in complex rotating plane:

$$\zeta = a + ib$$

Sign of spin is known, and can be distinguished by complex Fourier analysis

(includes frequency sign):

Signal vs non rotating effects at same frequency Violation signal appears in FFT⁻

An oscillating spurious effect at same frequency

only on one side of spin frequency line (left in case shown) at frequency distance ω_{orb} : $\zeta_{WEP} = \varrho_{WEP} e^{i(-\omega_{spin} - \omega_{orb})t}$

 ω_{orb} as the signal appears in FFT⁻ but on both sides of spin frequency line:

$$\zeta_{osc} = \frac{\rho_{osc}}{2} \left(e^{i(-\omega_{spin} - \omega_{orb})t} + e^{i(-\omega_{spin} + \omega_{orb})t} \right)$$

...read-out noise appears both in FFT⁻ and FFT⁺ (half each)...







Signal versus whirl motion

Whirl forward

Weak instability due to losses in the suspensions at spin frequency causing growing orbital motion of the

CM of test cylinders around common center of mass at the natural coupling frequency $\omega_w \simeq 10\omega_{orb}$ in the

same direction as spin

 $\zeta_{wf} = \varrho_{wf} e^{i(-\omega_{spin} - \omega_w)t}$

Line appears in FFT⁻ <u>left</u> of spin frequency, like signal but about 10 times farther away Whirl backward

Orbital motion of the CM of test cylinders around common center of mass at the natural coupling

frequency ω_w in the opposite direction w.r.t spin; damps naturally by physics laws

Line appears in FFT⁻ on the opposite side of the spin frequency line (to the <u>right</u>)

(same frequency, damps naturally)

 $\zeta_{wb} = \varrho_{wb} e^{i(-\omega_{spin} + \omega_w)t}$ This separation of lines is exploited in the control of whirl forward, to avoid amplifying whirl backward









Careful....

Not all systematics can be separated from signal this way...

Recipe on most dangerous systematics: have short integration time, have plenty of signal-to-noise ratio to burn (i.e. very low read-out noise), make many measurements to target sensitivity during mission lifetime, and then \Rightarrow let physics laws discriminate errors from signal...

... but this is another story...

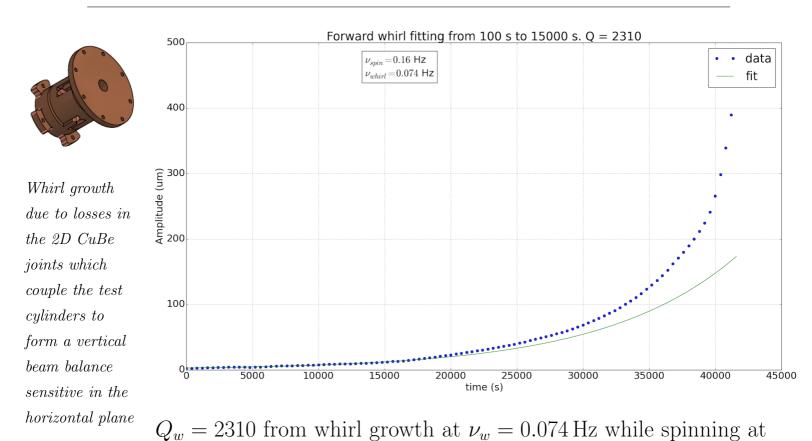


Pegna et al, PRL 2011, Nobili et al. PRD 2014





GGG prototype: Q measured from whirl growth



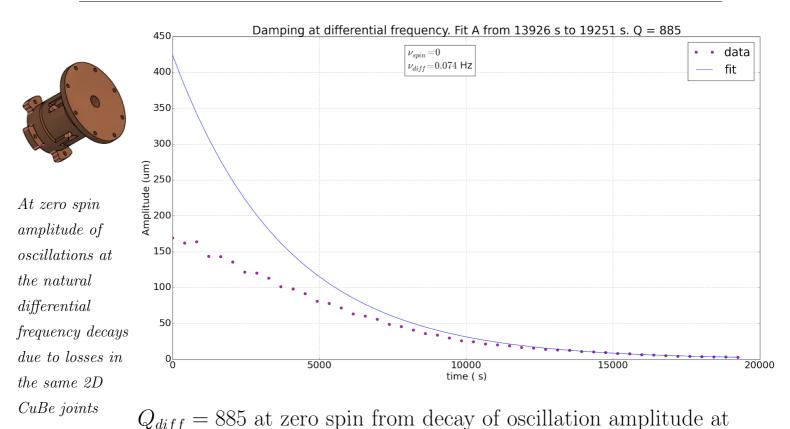


 $\nu_{spin} = 0.16\,\mathrm{Hz}$





GGG: Q from decay at $\nu_{diff} = \nu_w$, zero spin





Z. 1343

 $Q_{diff} = 885$ at zero spin from decay of oscillation ampl $\nu_{diff} = 0.074 \,\mathrm{Hz}$





Theory confirmed



- In low dissipation: $\nu_w = \nu_{diff}$
- Backward whirl damps naturally
- ullet Forward whirl growth depends on losses at spin frequency, not at natural differential (whirl) frequency \Rightarrow Q from whirl growth in rotation must be higher because spin frequency is higher than differential frequency and at higher frequencies losses are smaller

$$A(t) = A(t_o)e^{i(\omega_w(t-t_o)/2Q)} \qquad t - t_o = \frac{Q}{\pi}T_w \ln \frac{A(t)}{A(t_o)}$$

For GG sensor in space: Q=2310, whirl period $T_w = T_{diff} = 540 \,\mathrm{s} \Rightarrow$ once whirl has been damped a factor 10 growth needs 10.6 days!

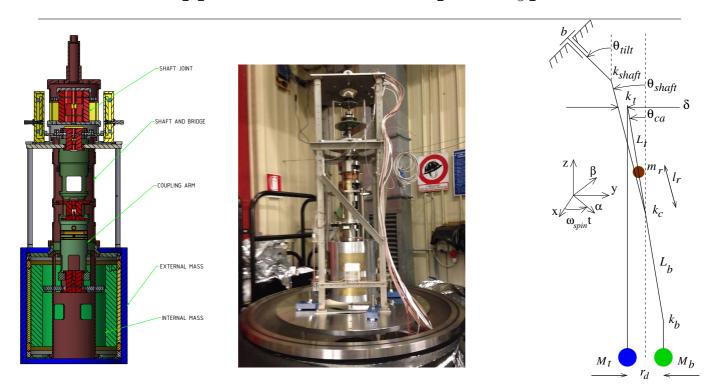
Q in GG will be higher because: i) much less complex flexures at zero g; ii) higher spin frequency; iii) smaller displacements. Requirement is Q = 20000 and bench tests give values close to it.







Application to GGG prototype



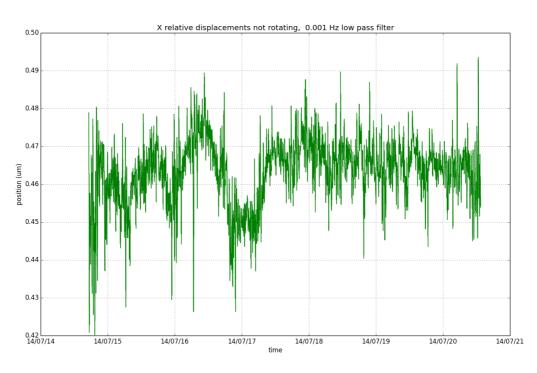
GG in space needs no motor no bearings, is isolated in space (no "terrain" tilts...), has weaker coupling and higher sensitivity by more than 3 orders of magnitude ... GG must deal with drag but know how is available...





Time series of relative displacements (I)





Time series of the relative displacements of the test cylinders; x axis of lab horizontal plane (non rotating frame).

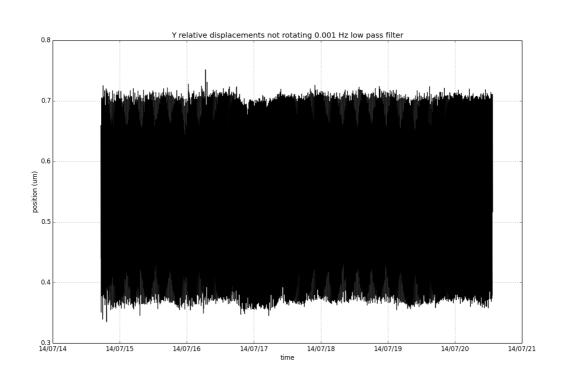
 $\nu_{spin} = 0.16 \,\mathrm{Hz} \; (\nu_{diff} = 0.074 \,\mathrm{Hz} \; \mathrm{natural} \; \mathrm{differential} \; \mathrm{frequency})$ The centers of mass stay within $0.08 \,\mu\mathrm{m}$ from each other.







Time series of relative displacements (II)



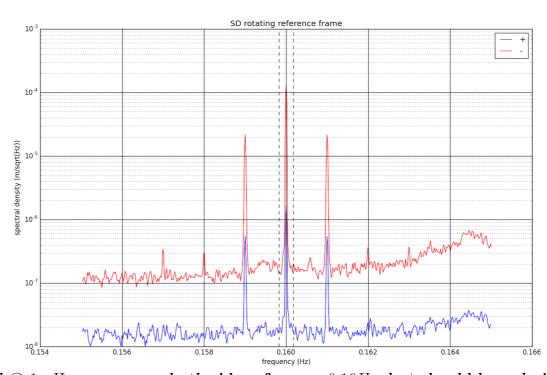
Time series of relative displacements along y axis of lab (non rotating frame) a 1 mHz. A calibration signal at 1 mHz is applied in y which dominates motion ...





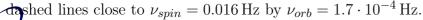


Complex Fourier analysis: Spectral Density



Applied signal @ 1 mHz appears on both sides of $\nu_{spin} = 0.16 \,\mathrm{Hz}$, but should be only in the red curve (SD⁺). Leakage to the blue curve (SD⁺) is due to bearings/motor rotation noise which makes "real" SD⁻, SD⁺ differ from ideal ones \Rightarrow bearings/motor rotation noise partially rejected in SD⁺.

GG in space has no motor/no bearings \Rightarrow blue (SD⁺) curve gives sensitivity to GG target signal at one of two

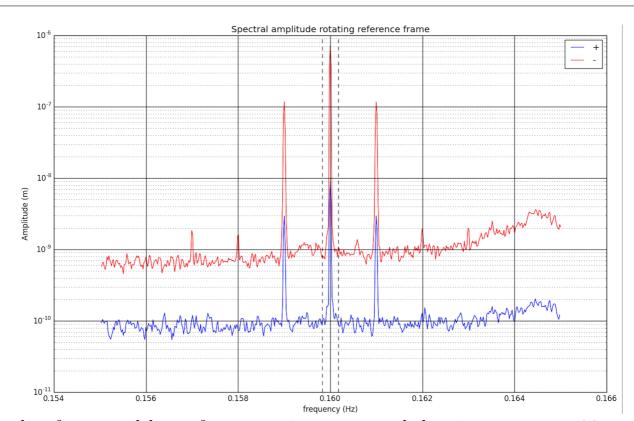








Complex Fourier analysis: spectral amplitude



Amplitude of spectral lines from previous spectral density: $\nu_{sampl} = 32\nu_{spin}$, $T_{res} = 86400 \, \mathrm{s}$









GGG current sensitivity (I)

- @ GG signal frequency $1.7 \cdot 10^{-4} \,\mathrm{Hz}$:
 - Lowest relative displacement/ $\sqrt{\text{Hz}}$ noise: $\simeq 2 \cdot 10^{-8} \,\text{m/}\sqrt{\text{Hz}}$
 - Lowest relative displacement noise (20 days): $\simeq 2.2 \cdot 10^{-11} \,\mathrm{m}$
 - Lowest relative displacement holse (20 days). = 2.2 10
 - Lowest differential acceleration noise/ $\sqrt{\text{Hz}}$ (with 0.074 Hz natural differential frequency): $\simeq 2 \cdot 10^{-8} \cdot (2\pi \cdot 0.074)^2 \, \text{ms}^{-2} / \sqrt{\text{Hz}} \simeq 4.3 \cdot 10^{-9} \, \text{ms}^{-2} / \sqrt{\text{Hz}}$
 - Lowest differential acceleration noise (20 days): $\simeq 4.76 \cdot 10^{-12} \,\mathrm{m/s^2}$









GGG: where does it stand as prototype of GG?

$$\eta_{GGGprototype@1.7\cdot10^{-4}\mathrm{Hz}} \simeq \frac{4.76\cdot10^{-12}\,\mathrm{m/s^2}}{8.1\,\mathrm{m/s^2}} \simeq 5.9\cdot10^{-13}$$

$$\eta_{GGGprototype@1.7\cdot10^{-4}Hz} = 10^{-17}$$
 $\eta_{GGGprototype@1.7\cdot10^{-4}Hz} = 7.0.10^4$

$$\eta_{GGtarget} = 10^{-17}$$

$$\frac{\eta_{GGGprototype@1.7\cdot10^{-4}Hz}}{10^{-17}} = 5.9 \cdot 10^{4}$$

$$\frac{sensitivityGG@zero-g}{sensitivityGGG@one-g} = (0.074 \,\text{Hz}/1.85 \cdot 10^{-3} \,\text{Hz})^2 = (540 \,\text{s}/13.5 \,\text{s})^2 \simeq 1600$$
no way to bridge this gap on ground!

$$\Downarrow$$

The only factor that GGG can still gain is: $\frac{5.9 \cdot 10^4}{1600} = 37$ (Note: target displacement signal in space is 0.6 pm and read-out noise must be $1 \text{ pm/}\sqrt{\text{Hz}} \otimes 1 \text{ Hz} \dots \text{ laser gauge, for other reasons too...}$







GGG: where does it stand compared to others?

Best GGG sensitivity to WEP/UFF violation in the field of the Sun (Nobili et al., CQG 2012):

$$\eta_{GGG_{\odot}@1.16\cdot10^{-5}\mathrm{Hz}} \simeq \frac{3.4\cdot10^{-10}\,\mathrm{m/s^2}}{a_{\odot-Pisa}} \simeq \frac{3.4\cdot10^{-10}\,\mathrm{m/s^2}}{0.0057\,\mathrm{m/s^2}} \simeq 6\cdot10^{-8}$$

GGG sensitivity to differential accelerations @ very low frequencies:

i)
$$6 \cdot 10^4$$
 times worse than torsion balances (...they cannot fly)

Braginsky & Panov, JEPT 1972 (Univ. Moscow) $\eta \simeq 10^{-12}$ (in the field of the Sun...) Baessler et al., PRL 1999 (UW Seattle, USA)

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$$\eta \simeq 10^{-12}$$
 (in the field

ii) 2.9 · 10³ times better than : Fray et al., PRL 2004 (Max Planck, DE) $^{85}\mathrm{Rb},\,^{87}\mathrm{Rb}$

Tarallo et al., 2014 ⁸⁵Sr, ⁸⁷Sr ...all at
$$\eta = 10^{-7}$$
 iii) 202 times better than Cs, SiO₂ test

Schlippert et al., PRL 2014 K, ⁸⁷Rb

Peters et al., Nature 1999 (Stanford, USA)

iv) 124 times better than ⁸⁷Rb, SiO₂ test

Carusotto, Polacco et al., PRL 1992 (CERN) Still the best test of WEP/UFF by mass dropping: $\eta = 7.2 \cdot 10^{-10}$!!!!

